



EURISOL DS PROJECT

MULTI-MW FISSION TARGET ISSUES

(Beam Window & Transverse Film Target)

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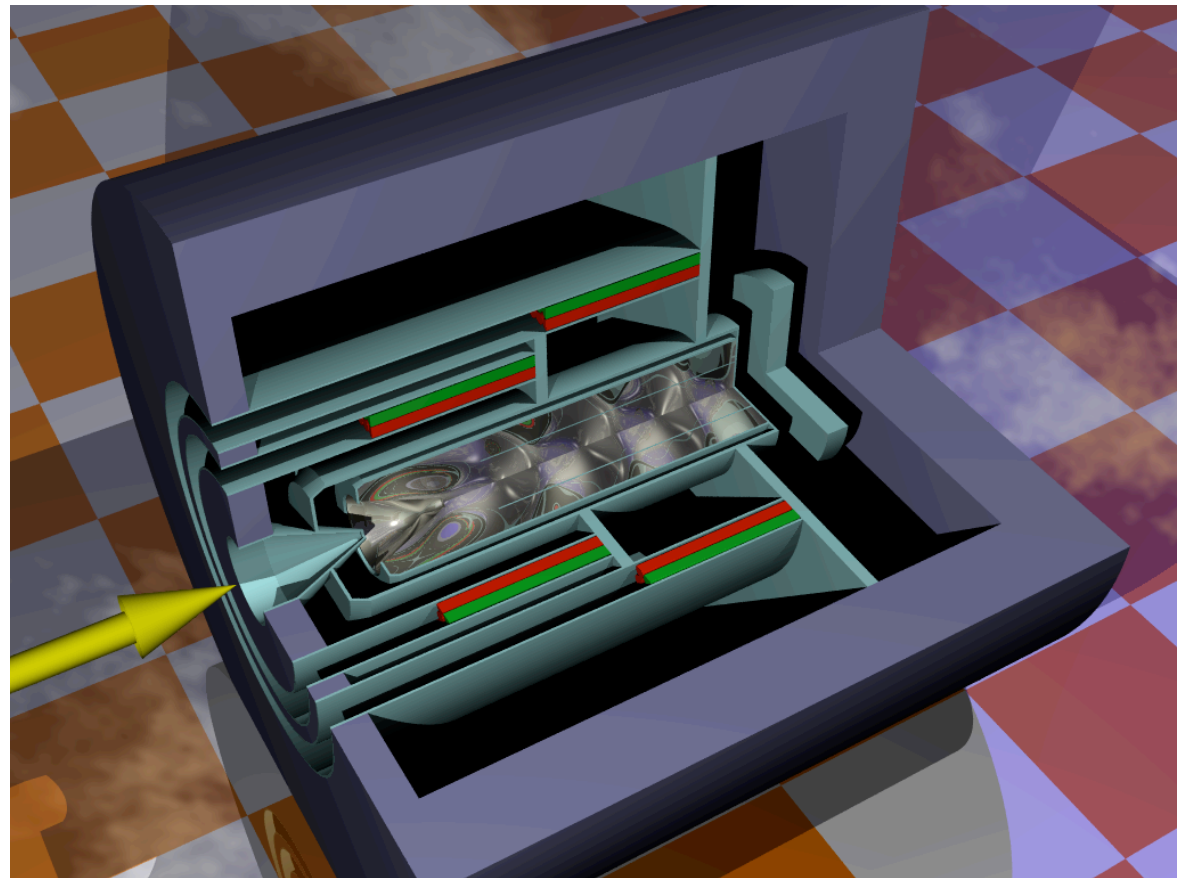
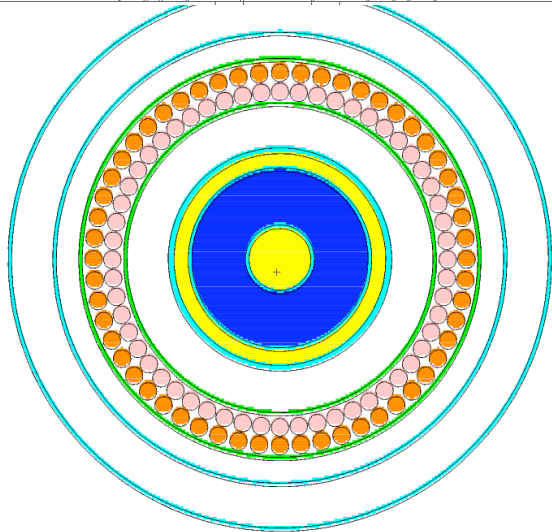
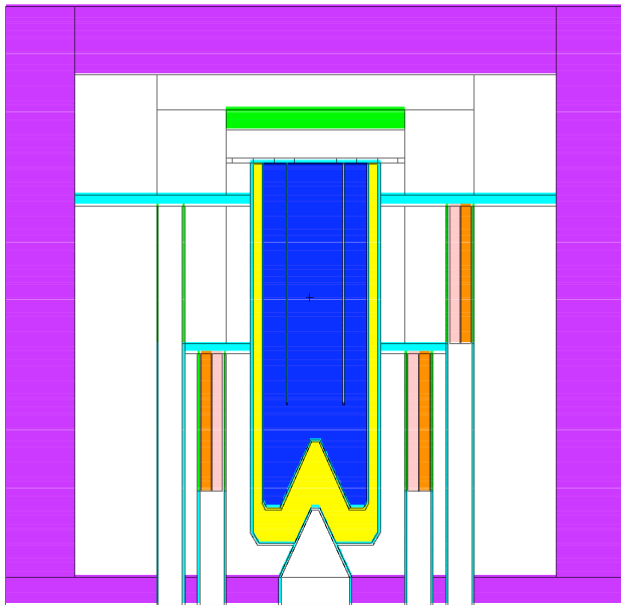
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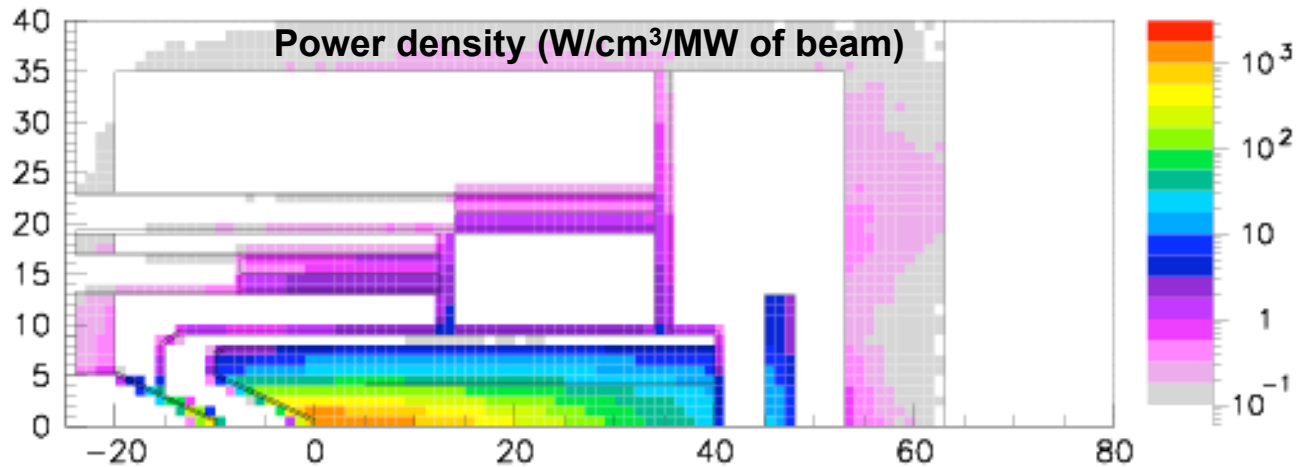
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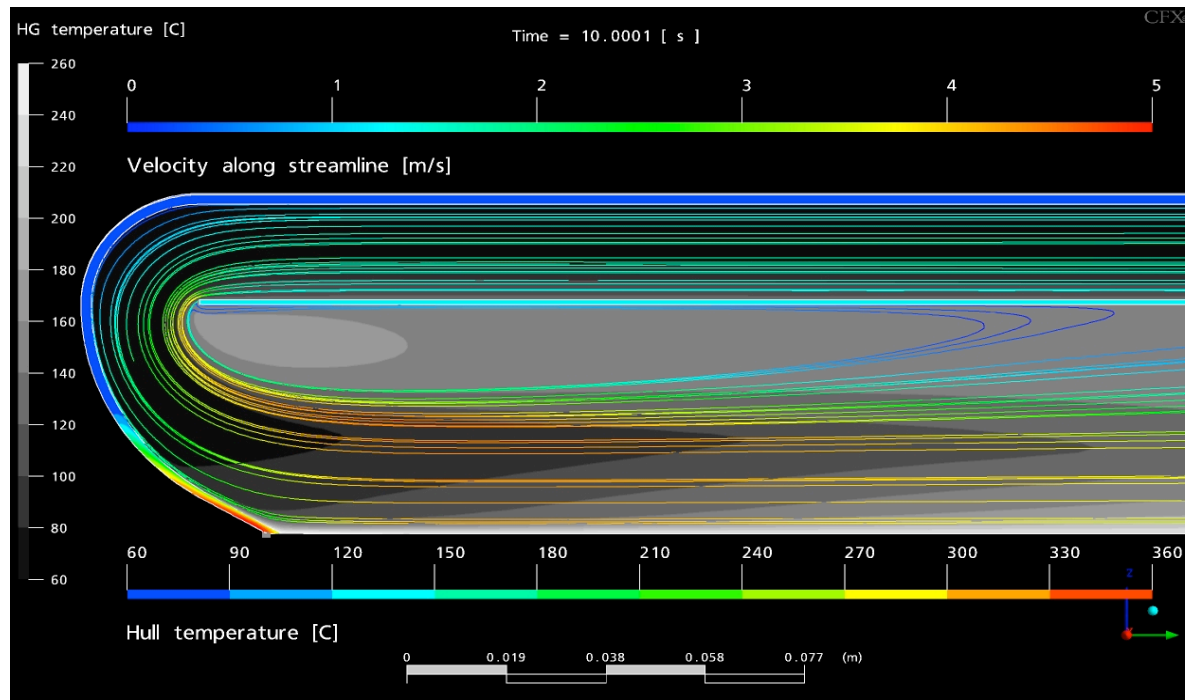
1. Larger Proton Beam
 - Beam Window Issues
 - Larger Proton Beam - Sigma = 25 mm
2. Transverse Film Windowless Target
 - Neutronic Parameters
 - Energy Densities
 - Fission Yields
3. Conclusions



- Reasonable charged particle confinement and power densities.
- High neutron fluxes, confined within the assembly.
- Large fission rate densities.
- Proven design (SNS and ESS), technically “simple” concept.



- Acceptable power densities in the Hg. Flow pattern not optimised; maximum temperature ~260 °C.

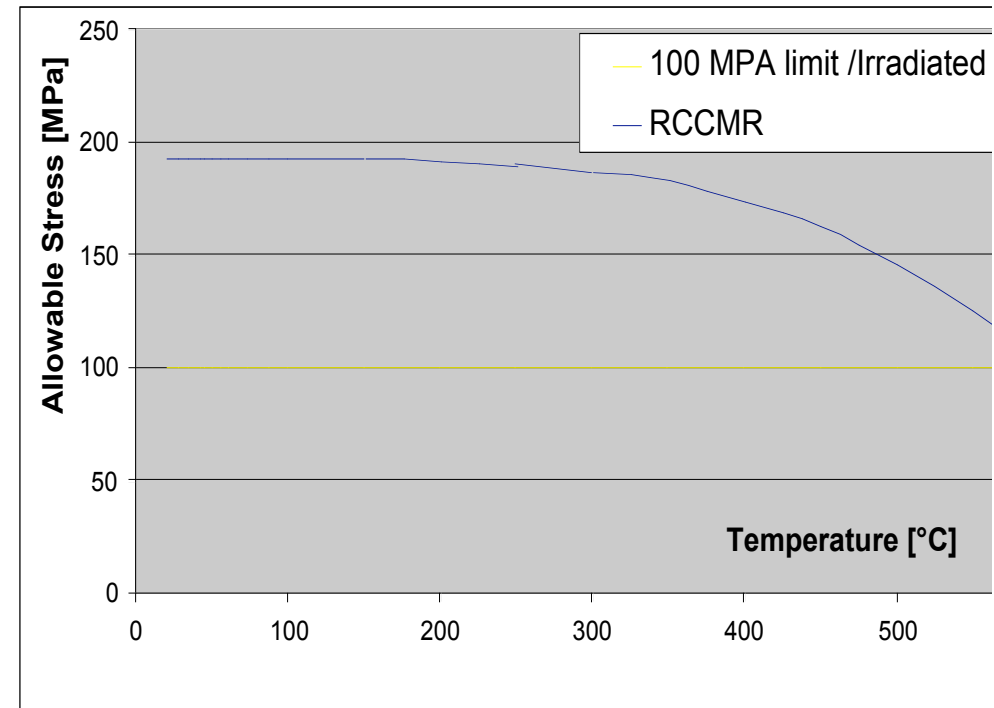
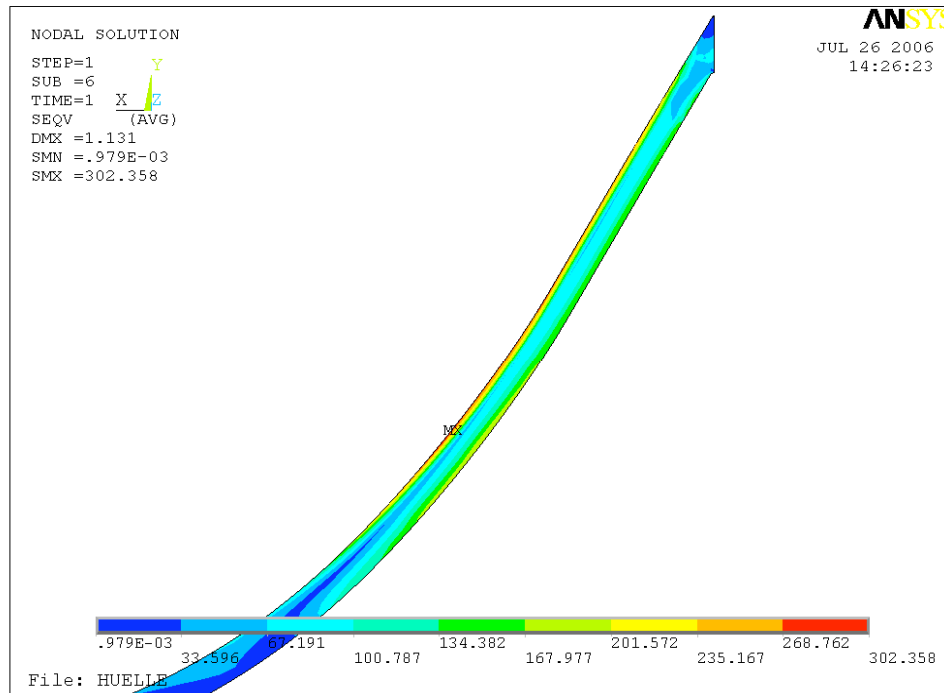


- Acceptable maximum temperature in the beam window (~350 °C).

- Large temperature gradient in the window, inducing mechanical stresses above the acceptance limits.



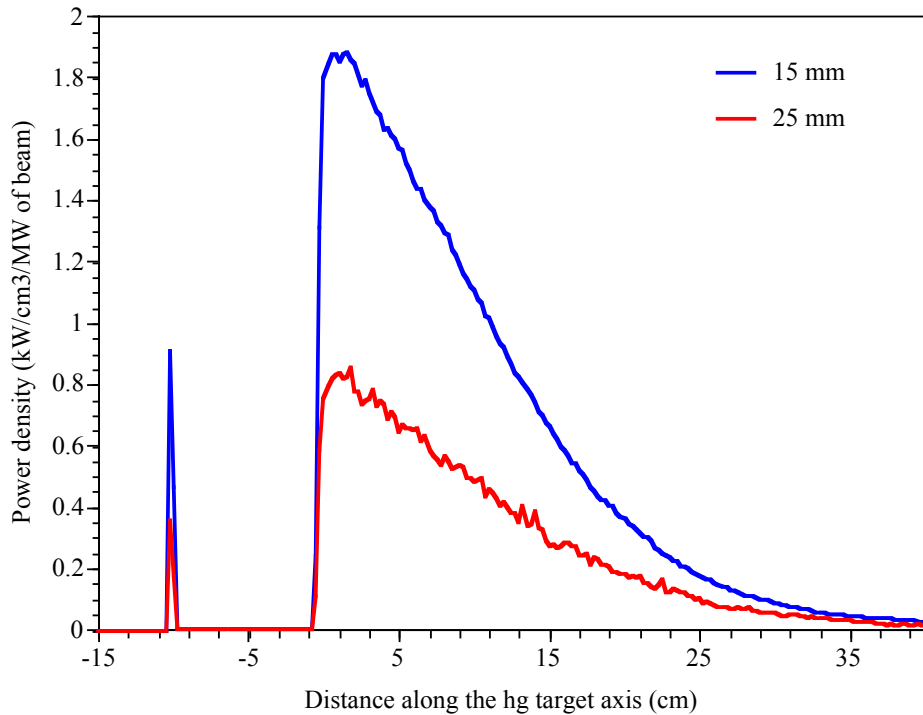
Results for outer annular inflow - Hg -Von Mises stress



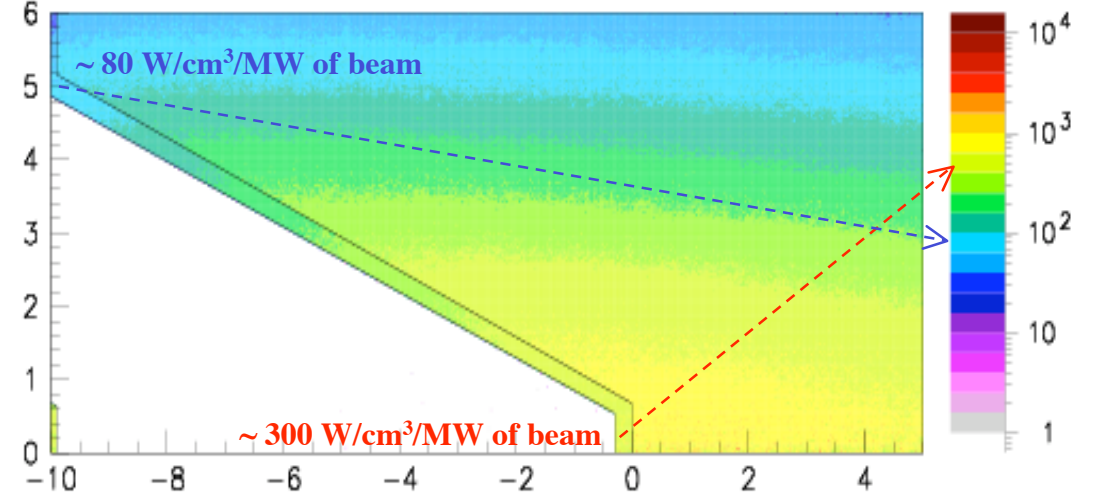
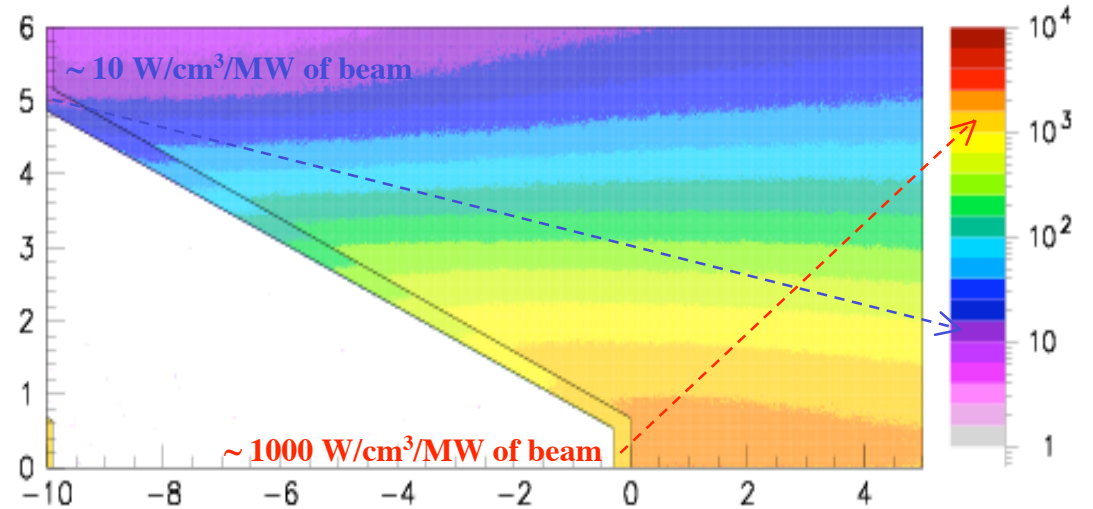
Resulting Von Mises stress in the beam window **~ 300 MPa**, considerably higher than the maximum allowable stress for irradiated steels (100 MPa). This is due to the greater thru-thickness temperature gradients along the beam window. **Possibility of cracking** due to tensile stress.



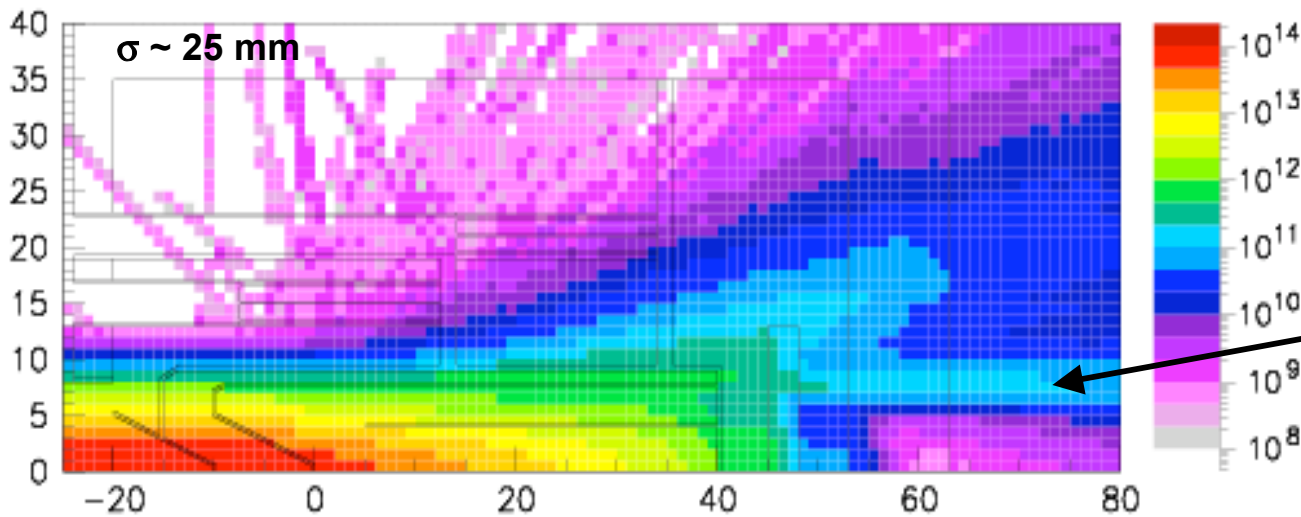
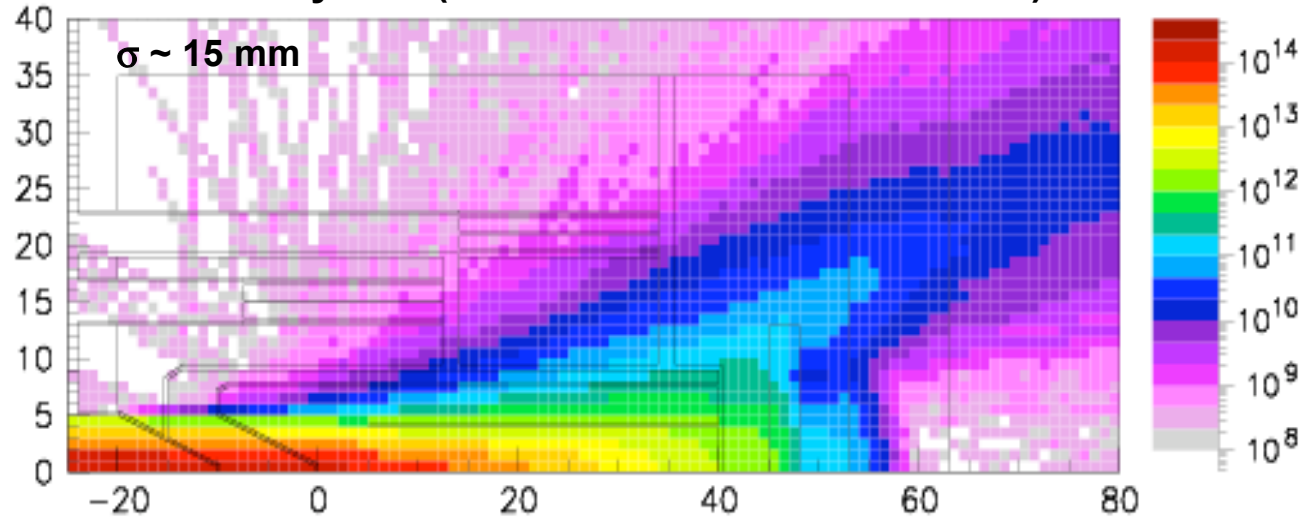
Energy Deposition in the Window



- Max. power density: 1.8 vs 0.8 (kW/cm³/MW of beam).
- Beam window: 0.9 vs 0.3 (kW/cm³/MW of beam).
- Significant differences in power density gradients in the beam window.

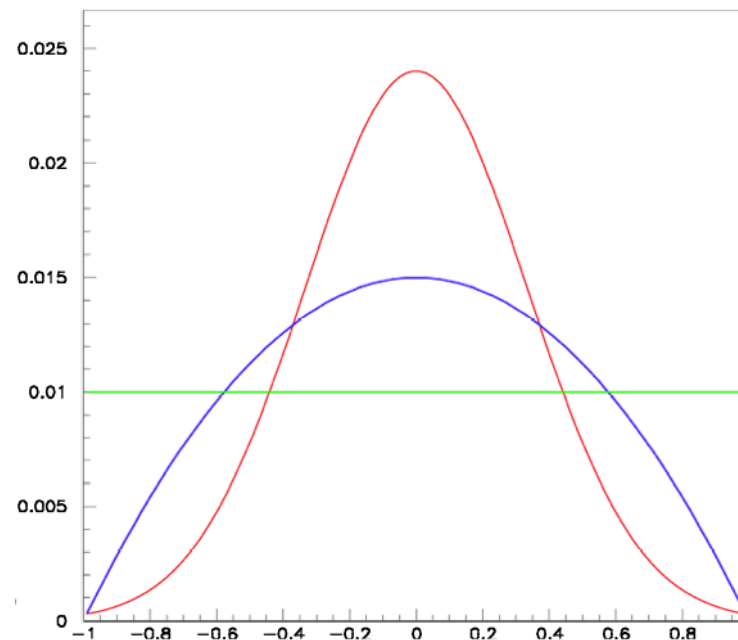


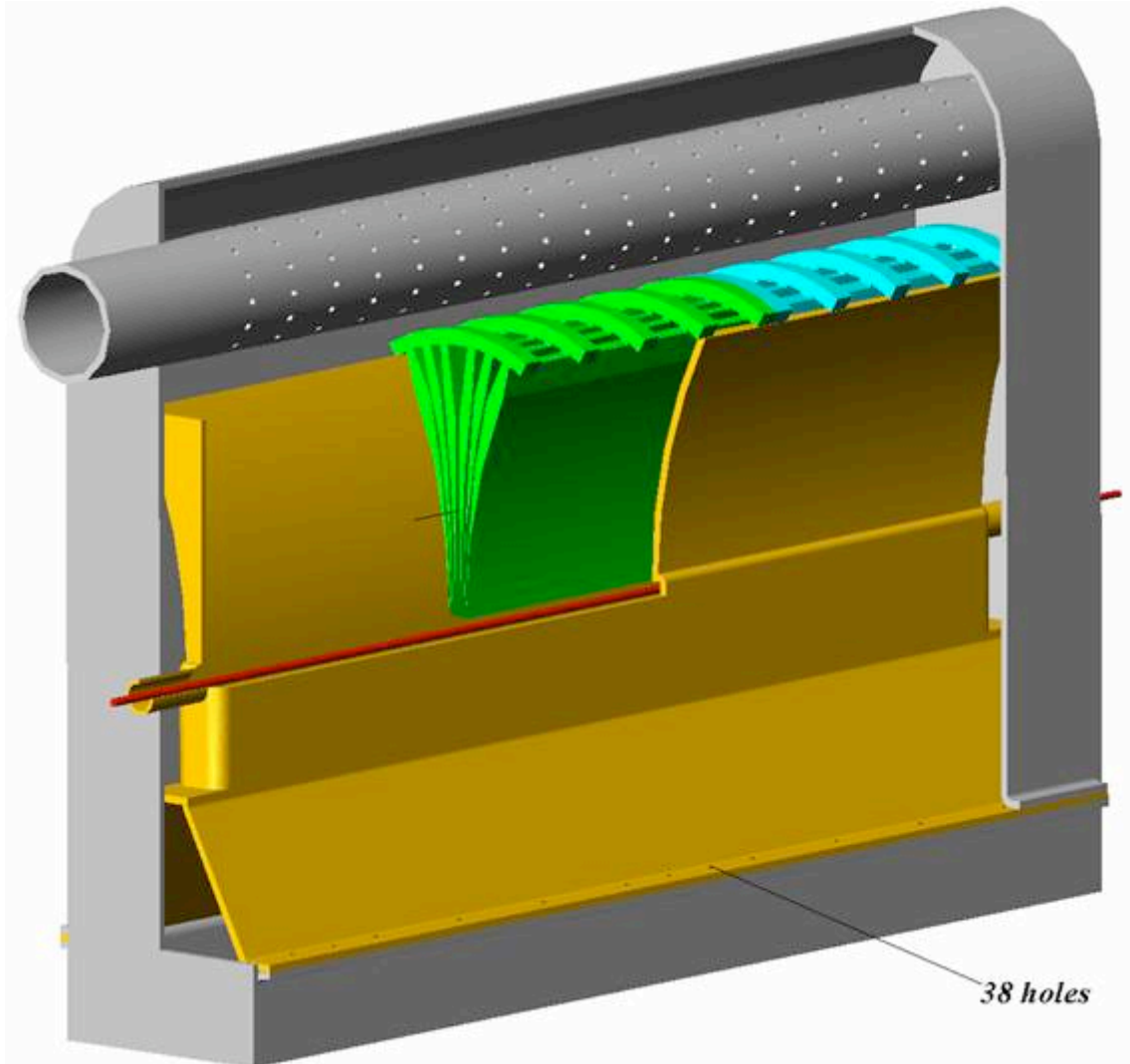
Primary flux (Primaries/cm²/s/MW of beam)



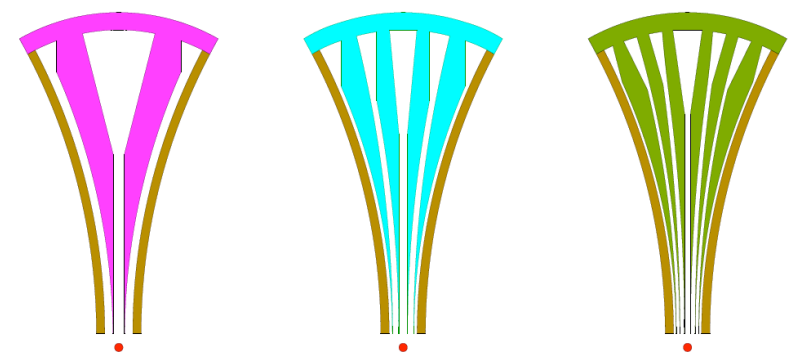
- Small primary contamination in the fission targets.
- Similar neutron fluxes.
- Some primary escapes at starting at $\sim 20 \text{ cm}$ from the impact point, from protons scattered at low angles.
- For $\sigma = 25 \text{ mm}$, primary proton streaming in the forward direction, along the Hg target surface.

- For a 15 mm Gaussian beam, power densities and temperature increase in the Hg flow stay below limits. Temperature gradients in the beam window produce unacceptable mechanical stresses, increasing the risk of breaking the window.
- A larger beam distribution, i.e. 25 mm, reduces the **power gradients** in the window but results in **high-energy proton escapes** in the forward direction. Need to optimise the geometry, work on the beam shape and provide a collimation system, to avoid proton streaming. A beam dump could also be foreseen.



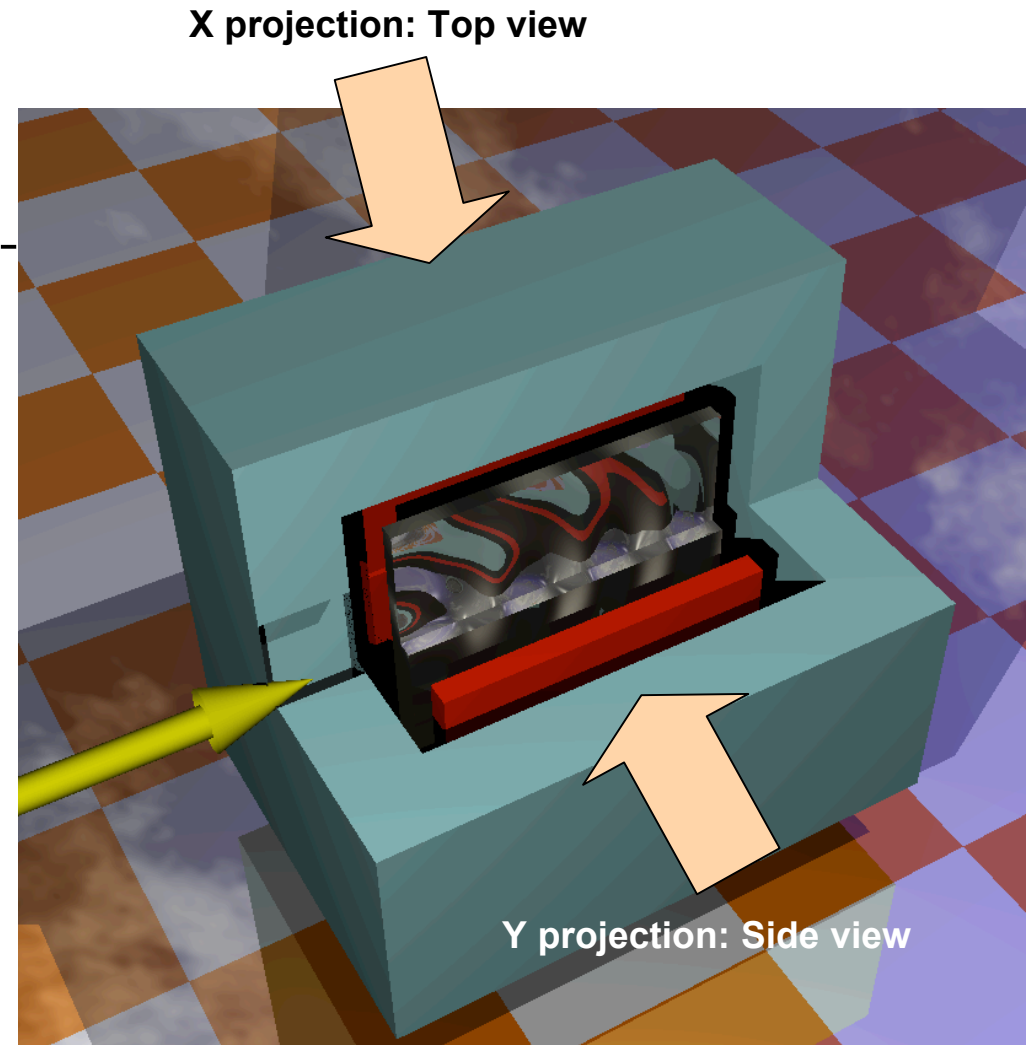
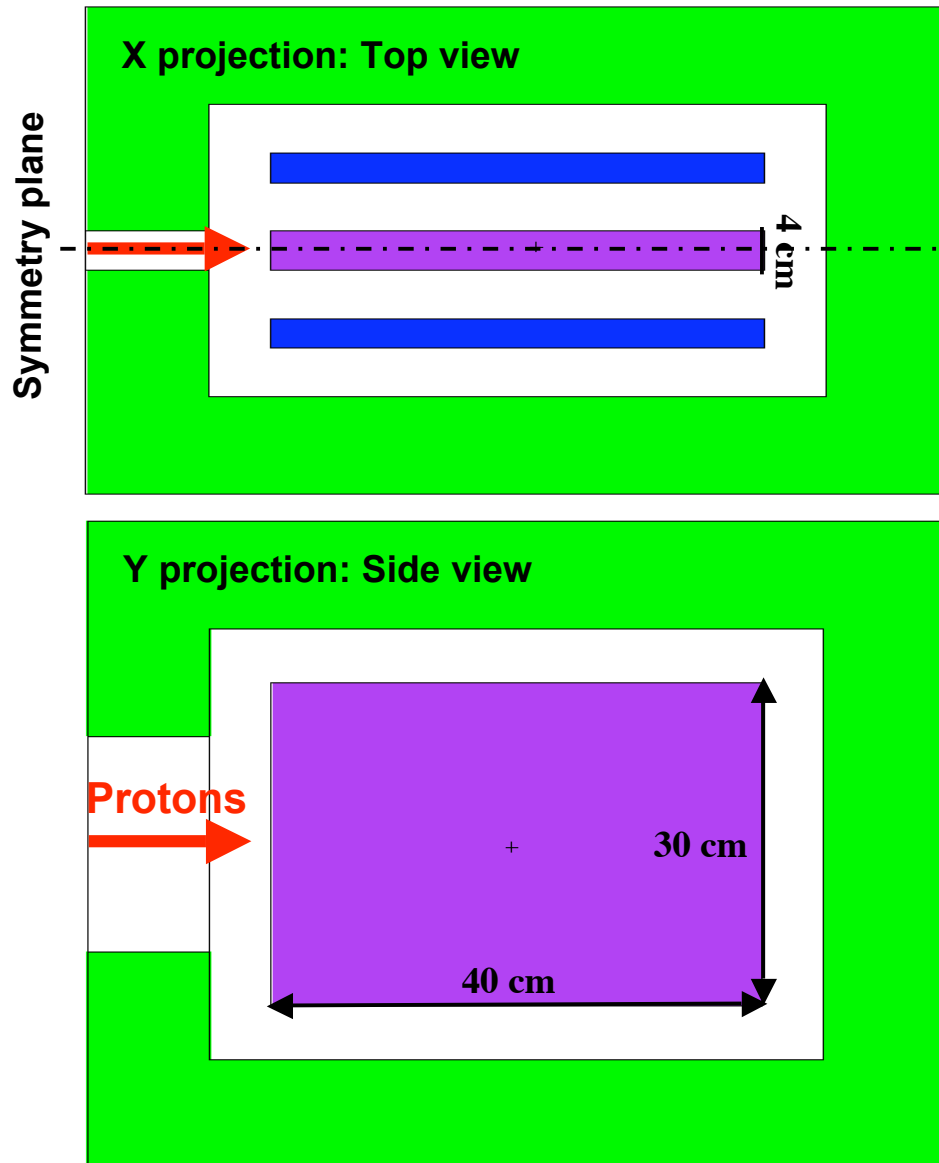


- Allows for different velocities in the Hg flow by changing the distance between of the flow-guides, according to the local heat deposition.
- Total Hg flow rate ~ 12 l/s.
Local velocity for a 3 mm gap ~ 4.4 m/s \rightarrow 118 K temperature increase for a beam $\sigma \sim 2$ mm.





Simplified Transverse Target Model



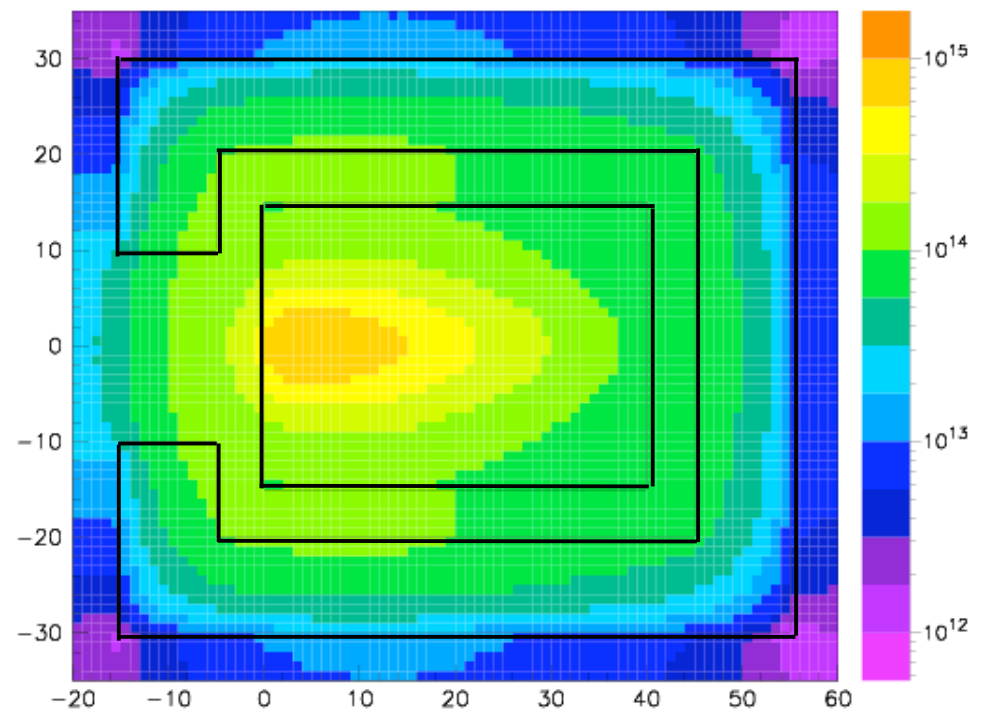
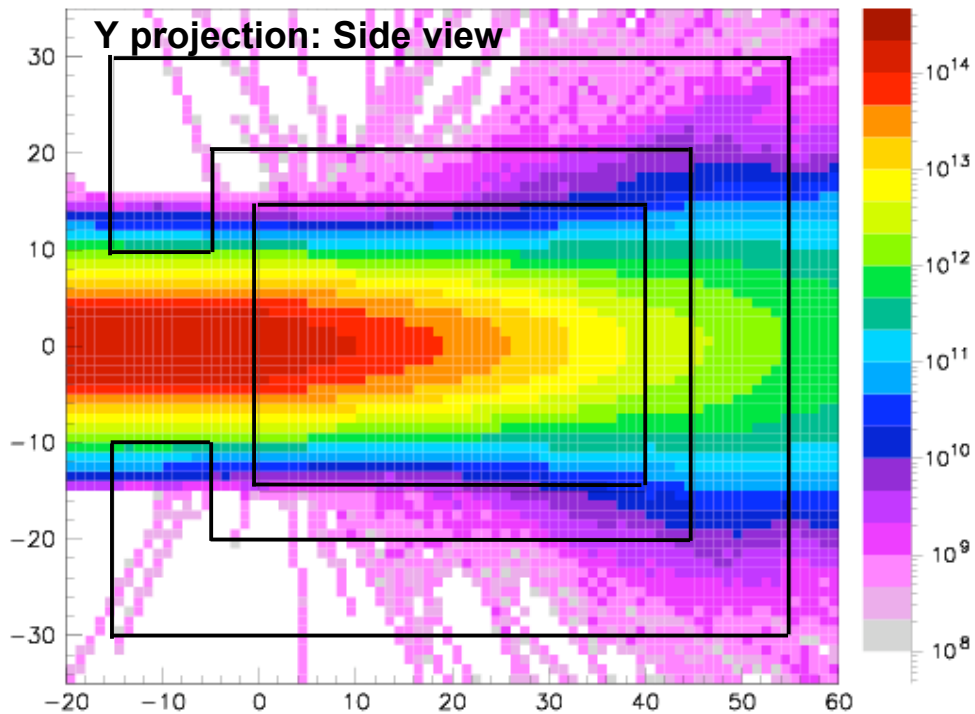
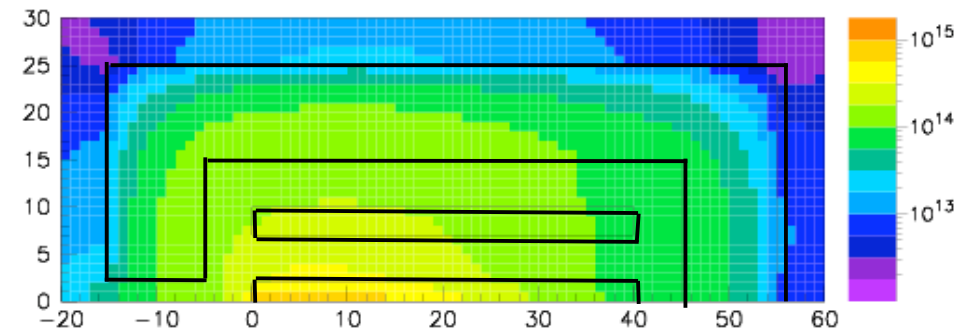
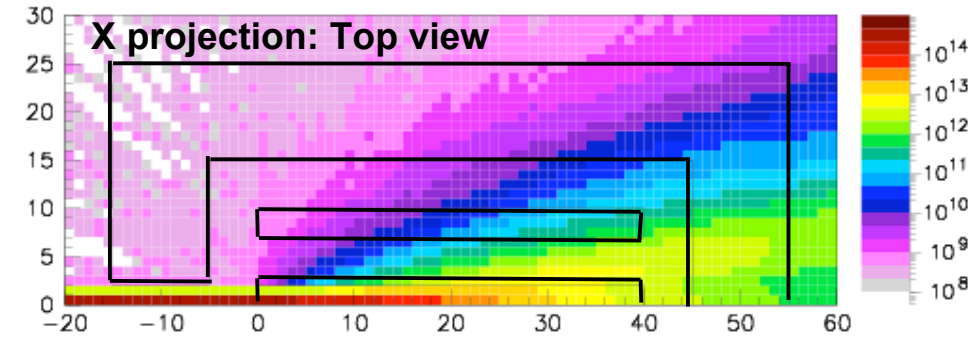
- Beam distribution: $\sigma_x \sim 4$ mm, $\sigma_y \sim 30$ mm



Primary and Neutron Distribution

Primary flux (Primaries/cm²/s/MW of beam)

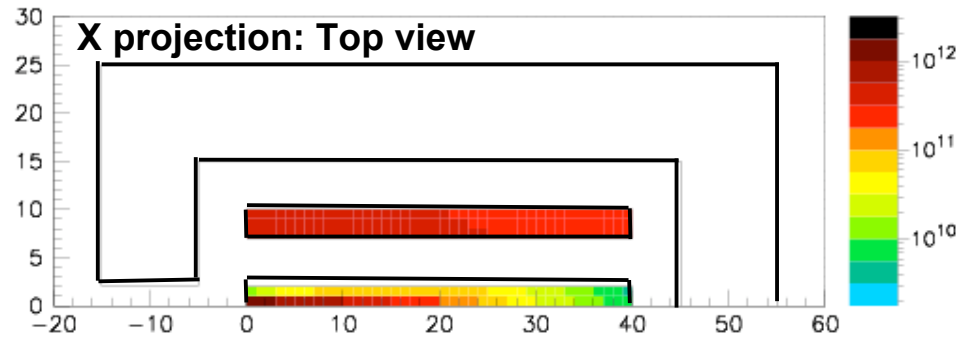
Neutron flux (Neutrons/cm²/s/MW of beam)



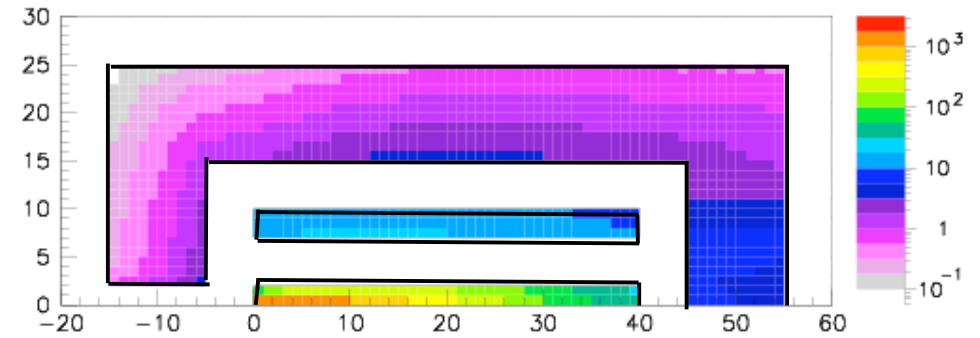


Neutron Balance, Fission and Power Densities

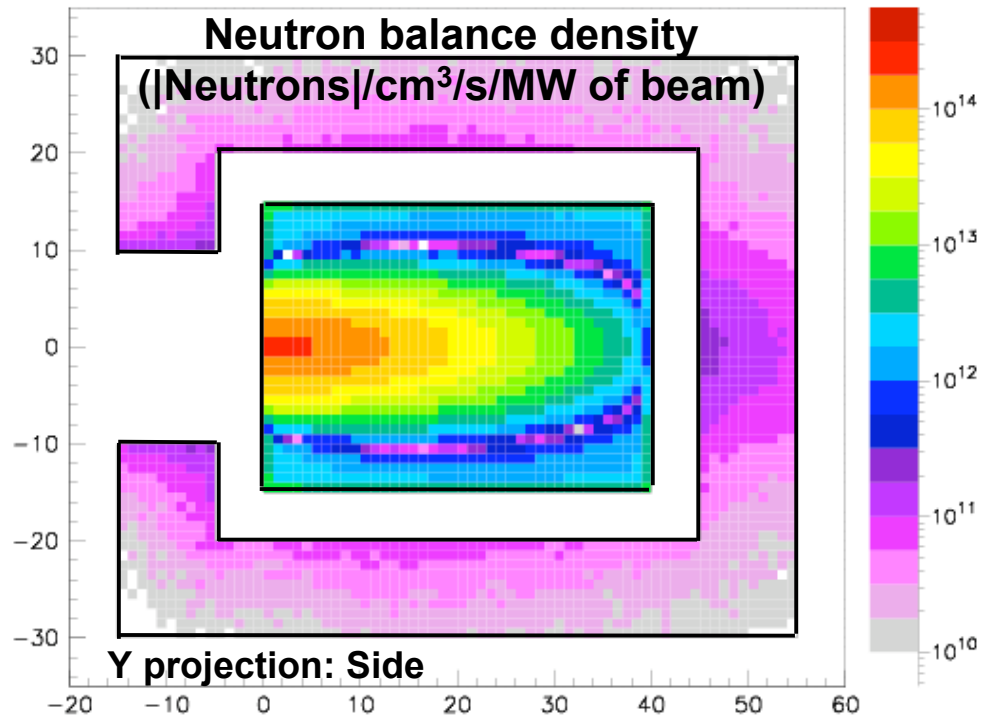
Fission density (Fissions/cm³/s/MW of beam)



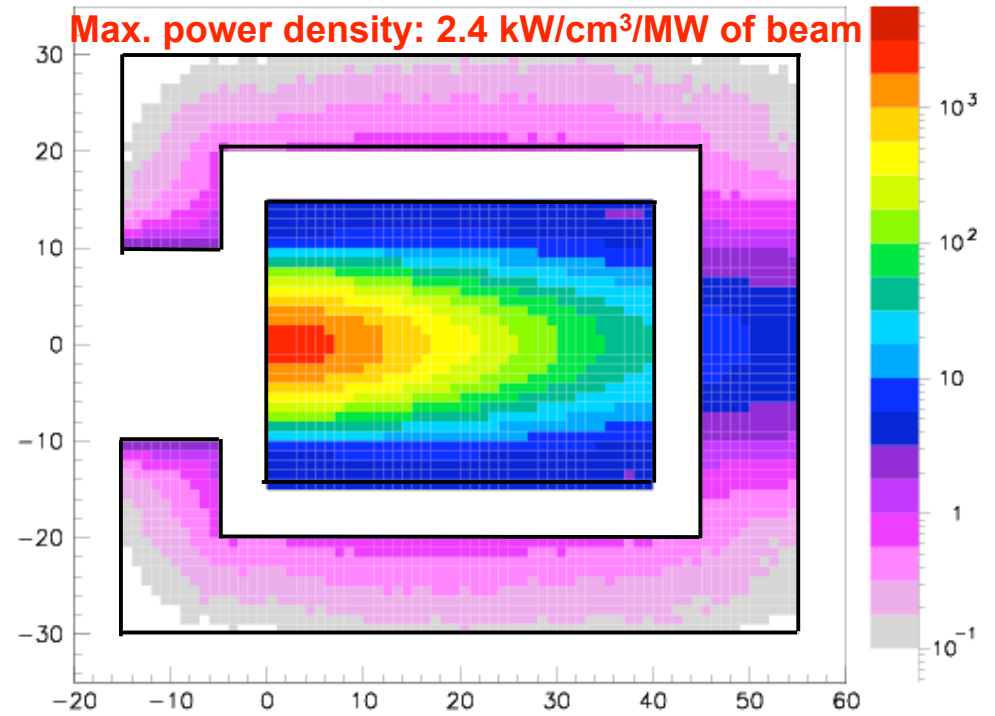
Power density (W/cm³/MW of beam)



Neutron balance density
(|Neutrons|/cm³/s/MW of beam)

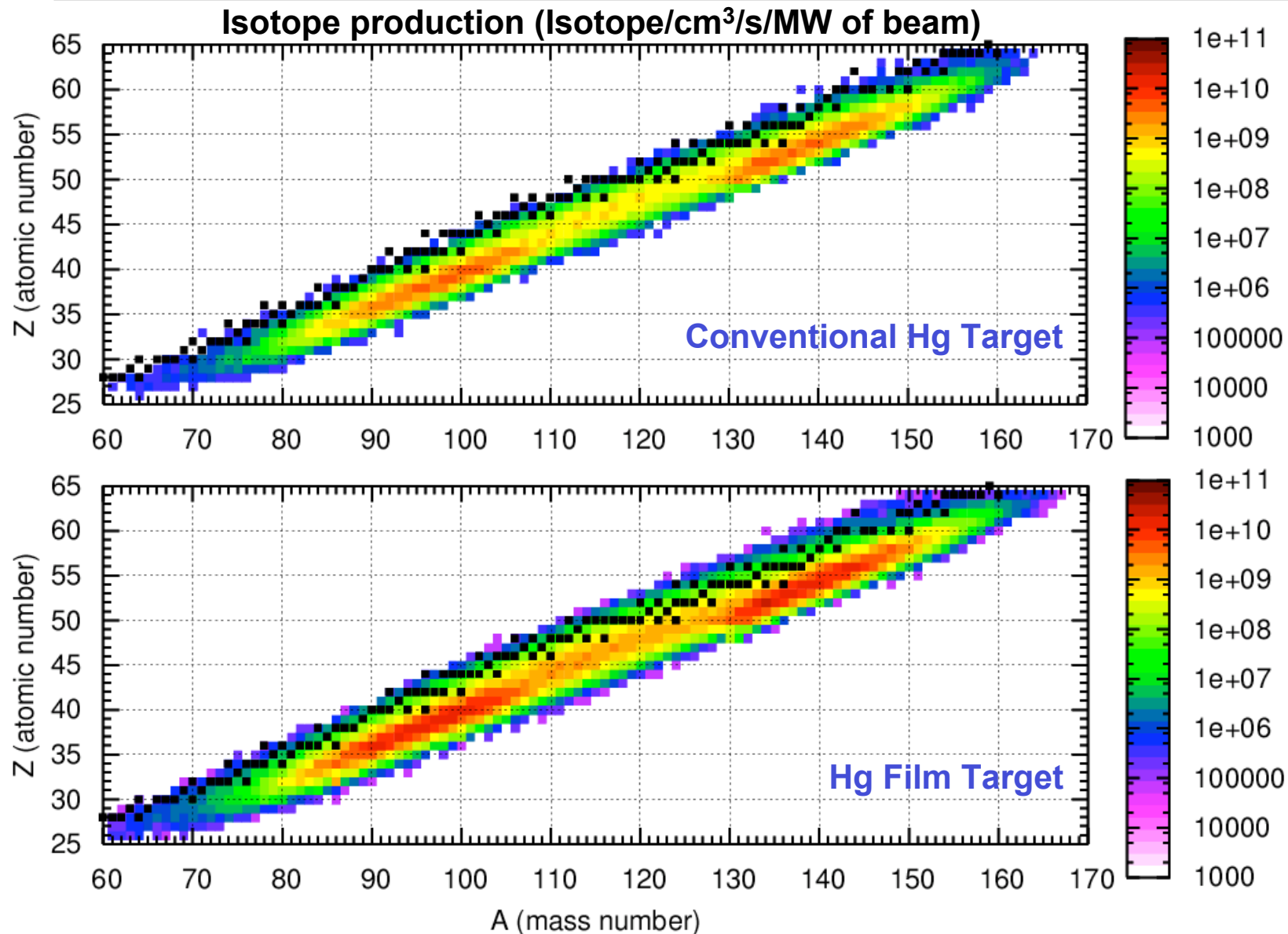


Max. power density: 2.4 kW/cm³/MW of beam





Radioactive Ions Production



UC₃ Targets:

- Natural Uranium (0.7% U-235)

- Density: 3 g/cm³



Conclusions

- The Hg film option presents a feasible alternative to the conventional target design, if the mechanical problems of the beam window remain unsolved.
- Small temperature increase in the Hg film at reasonable flow speeds.
- Important radioactive ion yields, similar to those in the Hg-jet, with a technically simpler solution.
- Large high-energy particle escapes, requiring a beam dump and improved shielding, due to the displaced neutron source. Radiation damage to nearby structures.